Design, Development and Optimization of S (-) Atenolol Floating Sustained Release Matrix Tablets Using Surface Response Methodology

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Gunjal, et al.: Floating Sustained Release Matrix Tablets of S (-) Atenolol

The objective of this present investigation was to develop and formulate floating sustained release matrix tablets of s (-) atenolol, by using different polymer combinations and filler, to optimize by using surface response methodology for different drug release variables and to evaluate the drug release pattern of the optimized product. Floating sustained release matrix tablets of various combinations were prepared with cellulose-based polymers: Hydroxypropyl methylcellulose, sodium bicarbonate as a gas generating agent, polyvinyl pyrrolidone as a binder and lactose monohydrate as filler. The 3^2 full factorial design was employed to investigate the effect of formulation variables on different properties of tablets applicable to floating lag time, buoyancy time, % drug release in 1 and 6 h (D_{1 h}, D_{6 h}) and time required to 90% drug release (t_{90%}). Significance of result was analyzed using analysis of non variance and *P* < 0.05 was considered statistically significant. S (-) atenolol floating sustained release matrix tablets followed the Higuchi drug release kinetics that indicates the release of drug follows anomalous (non-Fickian) diffusion mechanism. The developed floating sustained release matrix tablet of improved efficacy can perform therapeutically better than a conventional tablet.

Key words: Buoyancy time, floating lag time, floating sustained release, hydrophilic polymers, s (-) atenolol, surface response methodology

Beta blockers comprise a group of drugs that are mostly used to treat cardiovascular disorders such as hypertension, cardiac arrhythmia, and ischemic heart disease. Each of these drugs possesses at least one chiral center, and an inherent high degree of enantioselectivity in binding to the β -adrenergic receptor. For beta blockers with a single chiral center like atenolol, metoprolol, acebutolol, the (-) enantiomer possesses much greater affinity for binding to the β -adrenergic receptors than antipode^[1].

S (-) atenolol is a cardioselective β -1 adrenoceptor blocker devoid of intrinsic sympathomimetic and membrane-stabilizing activities. The maintenance of constant plasma level of a cardiovascular drug is important in ensuring the desired therapeutic response. Since the half-life of s (-) atenolol is 6–7 h, multiple doses are needed to maintain a constant plasma concentration for a good therapeutic response and improved patient compliance^[1]. Stoschitzky *et al.* study implied that the mean AUC, maximal plasma concentrations, t_{max} and plasma half-lives of the enantiomers were similar regardless of whether they were administered as optically pure enantiomers or as racemic mixture^[2-4]. Oral bioavailability of atenolol and its enantiomer is an about 50% since it has been reported that its absorption in the duodenum and jejunum is directly proportional to the dose availability^[5-7].

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A gastric floating drug delivery system (GFDDS) can overcome this problems and is particularly useful for drugs that are primarily absorbed in the duodenum and upper jejunum segments. The GFDDS is able to prolong the retention time of a dosage form in the stomach, thereby improving the oral bioavailability of the drug^[8-10].

Based on this, an attempt was made through this investigation to formulate floating sustained release tablet of s (-) atenolol by using hydroxypropylmethyl cellulose K15M (HPMC K15M) and hydroxypropylmethyl cellulose K100 LV (HPMC K100 LV) as a polymer. The 3² full factorial design was employed to investigate the effect of independent formulation variables, i.e. concentration of HPMC K15M and HPMC K100 LV on the various properties of tablets applicable to floating lag time (FLT), buoyancy time (BT), % drug release in 1 and 6 h (D_{1h}, D_{6h}) and time required to 90% drug release $(t_{00\%})$. The target release profile for proposed tablet formulation was calculated as per Robinson and Eriksen equation: After 1 h, 30-35% of the drug should be release; after 6 h, 60-65% of the drug should be release; and finally, till 12 h, the remaining drug should be release^[11].

MATERIALS AND METHODS

S (-) atenolol of Emcure Pharmaceutical Ltd., Pune, India was used. HPMC K15M, HPMC K100 LV kindly supplied by Colorcon Asia Pvt. Ltd., Goa, India. Sodium bicarbonate (SB), polyvinyl pyrrolidone K–30 (povidone K–30), lactose monohydrate (LM), magnesium stearate (MS), isopropyl alcohol (IPA), hydrochloric acid purchased from Cantan Lab, Baroda, India, BASF, Thane, India, Dynamix Dairy, Baramati, India, Nitika Pharmaceuticals, Nagpur, India, Deepak Fertilizers, Raigad, India and Merck, Germany, respectively.

Interaction study:

The possibility of any interaction between s (-) atenolol and excipients used in formulation of floating sustained release tablets was assessed by carrying out the differential scanning calorimetric (DSC) study. The thermal behavior of s (-) atenolol and its physical mixture, i.e., drug, polymers (HPMC K15M, HPMC K100 LV) and excipients (SB, LM, MS) were determined using DSC (Pyris 6 DSC, Perkin Elmer) at heating rate of 20°/min. The measurements were performed at a heating range of 50° to 200° under nitrogen atmospheres.

Full factorial design:

A two factor, three-level full factorial design (3^2) was employed for optimization of tablets. The concentration of HPMC K15M (A) and HPMC K100 LV (B) were selected as independent variables. Concentration of HPMC K15M was evaluated at 10, 15, and 20% of total tablet weight and the concentration of HPMC K100 LV was evaluated at 15, 20, and 25% of total tablet weight. The FLT, BT, D_{1 h}, D_{6 h} and t_{90%} selected as response (i.e. dependent variables). Design Expert 8.0.3. Software (Stat-Ease Inc., USA) was used for the generation and evaluation of statistical experimental design.

Formulation of floating sustained release matrix tablets:

Floating sustained release matrix tablets of s (-) atenolol were prepared by wet (non-aqueous) granulation according to the formula given in Table 1. S (-) atenolol (25 mg) was mixed with the required quantity of HPMC K100 LV and HPMC K15M in combination with SB (12.50 mg), and LM in rapid

TABLE 1: COMPOSITION OF FLOATING SUSTAINED RELEASE MATRIX TABLETS

Ingredients	Amount per tablet in mg								
	F1	F2	F3	F4	F5	F6	F7	F8	F9
S (-) atenolol	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00	25.00
LM	50.00	43.75	37.50	44.00	37.50	31.25	37.75	31.25	25.00
SB	12.50	12.50	12.50	12.50	12.50	12.50	12.50	12.50	12.50
HPMC K15M	12.50	12.50	12.50	18.75	18.75	18.75	25.00	25.00	25.00
HPMCK100LV	18.75	25.00	31.25	18.50	25.00	31.25	18.50	25.00	31.25
Povidone K 30	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00	5.00
IPA	Q.S.	Q.S.	Q.S.	Q.S.	Q.S.	Q.S.	Q.S.	Q.S.	Q.S.
MS	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1.25

HPMC K15M: hydroxypropyl methylcellulose K15M, HPMCK100LV: hydroxypropyl methylcellulose K100LV, LM: lactose monohydrate, SB: sodium bicarbonate, IPA: isopropyl alcohol, MS: magnesium stearate

mixer granulator for 30 min and then granulated with povidone K 30-IPA binder solution and dried in rapid fluidized bed dryer at 55° . The final granules were blended with MS (1% w/w) and compressed over 17 stations; single tooling tablet compression machine (Cadmach) using 7.7 mm flat faced beveled edge punches.

Characterization of granules:

When examining the flow properties of powder, it is useful to quantify the type of behavior in term of speed and more importantly uniformity of flow. Many different methods are available, either directly, using dynamic or kinetic methods, or indirectly, generally by measurements carried out on static beads. The powder properties include bulk density, tapped density and Carr's index was determined by procedure reported in USP 36.

Evaluation of floating sustained release matrix tablets:

The floating sustained release matrix tablets were evaluated for physical parameters, i.e., weight variation (BSA224S-CW, Sartorius balance), hardness (Monsanto hardness tester), thickness (Digital vernier caliper), friability (Friability test apparatus EF 2, Electrolab, India) and drug content.

Floating lag time and buoyancy time:

FLT and BT of the tablets were determined using USP 36 type II apparatus (Disso TDT 08 L, Electro lab) at 50 rpm in 900 ml using pH 1.2 buffer. The time in minutes taken by the tablet to reach the top from the bottom of the container was FLT and the time for which the tablet constantly floats on the surface of the medium was measured as BT.

In vitro release studies:

The *in vitro* drug release was studied by using USP 36 type II apparatus, i.e., Rotating paddle (Disso TDT 08 L, Electro lab). The dissolution was performed in 900 ml acidic buffer pH 1.2. The temperature was maintained at $37\pm0.5^{\circ}$ and the speed of paddle was kept at 50 rpm during dissolution study. Samples of 5 ml was collected at the interval of one hour and replaced with 5 ml buffer solution so as to maintained sink condition during study. The absorbance of samples was measured on UV spectrophotometer at 225 nm. The % drug release was calculated by DDSolver.

Kinetic modeling on drug release profile:

The nonlinear fitting of dissolution data was performed using DDSolver. The release mechanism and kinetics of the release profiles were analyzed by different mathematical models viz. zero order, first order, Higuchi, Hixson Crowell and Korsmeyer–Peppas models.

DDSolver provided a number of statistical criteria for evaluating the goodness of fit of a model, including the correlation coefficient (R obs-pre), the coefficient of determination (Rsgr, R^2 , or COD), the adjusted coefficient of determination (Rsqr adj or R² adjusted), the mean square error (MSE), the standard deviation of the residuals (MSE root or Sy.x), sum of squares (SS), weighted of sum of square (WSS), the Akaike information criterion (AIC), and the model selection criterion (MSC). Among these parameters, the most popular ones in the field of dissolution model identification are the R² adjusted, the AIC, and the MSC^[12]. Korsmeyer-Peppas model is used to analyze the release of pharmaceutical polymeric dosage forms, when the release mechanism is not well known or when more than one type of release phenomena could be involved^[13].

Statistical analysis of the data and optimization:

The best fitting model was selected based on the comparison of statistical parameters including the coefficient of variation (CV), the coefficient of determination (R^2), adjusted coefficient of determination (adjusted R^2) and the predicted residual sum of square (PRESS) provided by Design Expert software. In addition, statistical analysis like ANOVA to identify significant effect of factors on response, regression coefficients, F test and P value were also calculated with the software.

The relationship between the dependent and independent variables was further elucidated by using response surface plots. These plots are useful in the study of effects of formulation factors on the response at one time and predict the responses of dependent variables at the intermediate levels of independent variables. Subsequently, a numerical optimization technique by the desirability approach and graphical optimization technique by the overlay plot were used to generate the new formulations with the desired responses^[14].

RESULT AND DISCUSSION

S (-) atenolol oral bioavailability has been reported to be about 50%, perhaps because of rapid hepatic firstpass metabolism. S (-) atenolol has narrow absorption window in the small intestine. If the s (-) atenolol dosage form can be retained in the stomach as long as possible, to allow for maximum absorption, s (-) atenolol bioavailability can be improved. GFDDS is one approach; in it, the gastro intestinal residence time is prolonged because of the floating behavior^[15,16]. Floating matrix tablets were formulated as per 3² factorial design, and the sustained release polymer concentration was considered to have a significant effect on the release from the HPMC matrices, as increase or decrease in polymer concentration affects gel strength of matrix tablet. HPMC was chosen because it swells rapidly when come in contact with water; upon contact with water, a hydrogel layer would be formed to act as a gel boundary for the delivery system. HPMC K15M and HPMC K100 LV were used as swellable polymers. As s (-) atenolol is highly water soluble drug, to control burst release from matrix, low viscosity grade of HPMC, i.e., HPMC K100 LV used. Since HPMC K100 LV comes in contact with dissolution media start to swell immediately as compared to HPMC K15M^[17].

The DSC curve of pure s (-) atenolol showed characteristic sharp endothermic peak at 157.54°, indicating the melting point of the drug (fig. 1). The obtained DSC curve for physical mixture of drug with excipients shows the endothermic peak at 153.83° of s (-) atenolol. No change in the endotherm of the drug was observed in the physical mixture. This implied that there was no interaction between the drug and excipients.



Fig. 1: DSC thermogram. DSC thermogram of (a) S (-) atenolol. (b)

DSC thermogram of (a) S (-) atenolol, (b) excipients (placebo) and (c) its physical mixture.

Matrix tablets were formulated according to wet granulation method as described in Table 1. Granulation is the key process in the production of matrix sustained release dosage form. The properties of granules which should be evaluated to ensure the proper formulation of the tablet dosage form is an important aspect in matrix tablet formulation. The results reported in Table 2 inferred that the granules prepared by nonaqueous granulation were considerably good to formulate tablets.

The percentage weight variation of individual tablets from the average weight was found within \pm 7.5% (w/w) which evidenced that the entire tablets complies the IP weight variation test (Table 3). The tablet hardness of entire batches was found in the range of 3.36 \pm 0.61 kg/cm²-5.12 \pm 0.89 kg/cm² (Table 3). The Percentage weight loss of the tablet was measured and found in the range of 0.09–0.18%. It implied that tablet has good strength (Table 3). Size of tablets was found 7.72 \pm 0.1 mm in diameter, and thickness of that tablet was found 3.07 \pm 0.08–3.17 \pm 0.09 mm. The size and thickness of tablets were uniform; it indicated that uniform and proper filling of granules into the dies during compression of tablet.

Drug content in the tablet was reported in Table 3 which complied as per IP general monograph. The result indicated that in all formulation s (-) atenolol was uniformly distributed. The *in vitro* buoyancy study of floating sustained release matrix tablets of different formulation batches are shown in Table 4. Floating lag time of factorial sustained release matrix tablet was found in the range of 78 to 306 s. The formulation containing higher concentration of HPMC K100 LV showed least FLT. This was might be due to the faster swelling rate of HPMC K100 LV compared to HPMC K15M. The gas generated

TABLE 2: PROPERTIES OF GRANULES READY FOR
COMPRESSION

Formulation	Bulk	Tapped	Carr's	Angle of	
	density (g/ml)	density (g/ml)	index (%)	repose	
F1	0.754±0.07	0.878±0.05	14.12±0.06	32.80±0.11	
F2	0.781±0.09	0.899±0.09	13.12±0.05	30.06±0.08	
F3	0.784±0.09	0.930±0.11	15.68±0.09	31.33±0.16	
F4	0.735±0.12	0.854±0.08	13.93±0.06	32.97±0.12	
F5	0.764±0.14	0.891±0.09	14.25±0.13	30.68±0.09	
F6	0.782±0.08	0.936±0.08	16.45±0.08	32.16±0.11	
F7	0.767±0.09	0.913±0.13	15.99±0.11	31.83±0.12	
F8	0.781±0.12	0.927±0.09	15.74±0.05	31.62±0.09	
F9	0.792±0.15	0.943±0.11	16.01±0.05	30.85±0.13	

TABLE 3: CHARACTERISTIC PROPERTIES	OF FLO	ATING SUSTAINED	RELEASE MATRIX	TABLETS
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Formulation	Average weight (mg)	Hardness (kg/cm²)	Thickness (mm)	Friability (%)	Drug content (%)
F1	125.26±0.64	3.87±1.17	3.12±0.07	0.17±0.04	101.03±0.31
F2	126.63±0.91	3.36±0.61	3.17±0.05	0.12±0.12	99.86±0.70
F3	124.87±1.02	4.51±0.29	3.10±0.11	0.17±0.08	99.27±1.02
F4	125.67±0.83	4.26±0.38	3.07±0.08	0.12±0.09	99.61±0.73
F5	124.26±0.61	4.69±0.41	3.13±0.08	0.09±0.06	99.83±0.41
F6	125.71±0.90	5.12±0.89	3.16±0.07	0.11±0.07	100.83±1.13
F7	124.36±1.24	3.92±0.67	3.17±0.09	0.18±0.15	98.94±0.42
F8	125.12±1.61	5.03±0.78	3.11±0.12	0.12±0.08	101.02±1.1
F9	126.87±1.02	4.21±1.29	3.08±0.07	0.13±0.11	99.57±0.70

TABLE 4: FLT AND BT

Formulation	FLT (s)	BT (min)
F1	78±0.07	578±0.51
F2	103±0.10	596±0.42
F3	159±0.12	581±0.67
F4	197±0.08	697±0.17
F5	232±0.13	706±0.78
F6	268±0.09	718±0.41
F7	284±0.11	789±0.12
F8	306±0.07	809±0.14
F9	347±0.17	814±0.09

FLT: floating lag time, BT: buoyancy time

is trapped and protected within the gel formed by hydration of polymer, thus decreasing the density of tablet. As the density of tablet falls below 1 the tablet becomes buoyant. The buoyancy time of the formulation was affected with the variation in polymer concentration^[17]. The buoyancy time of the formulation significantly affected by change in concentration of HPMC K15M compared to HPMC K100 LV. HPMC K15M plays significant role in buoyancy as it has higher viscosity and slow erosion rate compared to HPMC K100 LV. As dissolution media permeates into core of the matrix, gel layer (rubbery state) grows with time, increasing the thickness of the gel layer entraps carbon dioxide for more time^[18]. The optimized factorial batch was characterized for floating behaviour in 50 ml of 0.1 N hydrochloric acid and its observation shown in fig. 2.

The *in vitro* drug release profile of floating sustained release matrix tablet represented in fig. 3. The release profile revealed that increase in polymer concentration slower the drug release. The increase in polymer proportion resulted in increase in viscosity of the tablet matrix gel layer as well as formation of a gel layer with a longer diffusional path. This phenomenon resulted in decrease effective diffusion of the drug and therefore a reduction in drug release rate. The increase in HPMC K15M concentration significantly



Fig. 2: Floating behavior of optimized factorial batch (I). Tablet at initial level, (A) tablet at 1 h, (B) tablet at 4 h, (C) tablet at 8 h, (D) tablet at 12 h.

slower the drug release compared to increase in concentration of HPMC K100 LV. This result revealed that a polymer of higher viscosity induces greater chain entanglement than a polymer of low viscosity. Therefore, it is harder for longer chains to dissolve because of the high energy required for pulling them off the matrix. Thus, higher viscosity polymers induce the formation of a thicker gel layer after hydration^[18].

The release profile of all factorial batches implied that at initial level drug release faster and decrease in the release rate with time. This is might be due to at an early time, drug close to matrix surface might be released before the surrounding polymer reached the polymer disentanglement concentration (the concentration of the polymer in a fully hydrated state at which there are no polymer–polymer interactions) because the diffusion coefficients for drug molecules were higher than the polymer. Especially, the high viscosity polymers would take longer time to form a gel layer, within this time; major amount of the drug might have been released^[19,20]. The increase in HPMC K100 LV concentration significantly reduces burst release of s (-) atenolol at initial level. This might be due to the faster swelling of HPMC K100 LV forms gel layer at surrounding.

The release profile and kinetics of drug release are important because they correlate the *in vitro* and *in vivo* drug responses by comparing results of pharmacokinetics and dissolution profile patterns. Hence, the cumulative drug release results of factorial batches were fixed into different mathematical models. The dissolution modeling gives guidance for identifying best fit model which remarked as, the best fit model should be the one with the highest R² adjusted, should have MSC value more than two to three and should have lower AIC value.



Fig. 3: Comparative release profiles of floating sustained release matrix tablets. → F1, → F2, → F3, → F4, → F5, → F6, → F7, → F8, → F9.

It can be highly postulated that in vitro release profile of all matrix formulation could be best expressed by the Higuchi model (Table 5). The plot showed high linearity in comparison to other release kinetic equations. Release of drug from the matrix tablet generally follows diffusion for water soluble drug and erosion or relaxation for water insoluble drug. Diffusion is related to transport drug from the dosage matrix into the in vitro study fluid depending on the concentration gradient between dosage form and in vitro fluid. As gradient varies, the drug is released and the distance for diffusion increases. This could explain why the drug diffuses at a comparatively slower rate, as the dissolution time increases which is referred as square root kinetics or Higuchi kinetics. To confirm diffusional mechanism, the data were fitted into Korsmever et al.'s equation (Table 6). For matrix tablet, n value 0.5 indicates diffusion controlled value to near 1.00 indicates erosion. Intermediate value suggests simultaneous diffusion and erosion contribute to overall release mechanism^[21].

Polynomial models including linear, interaction and quadratic terms were generated for response variables using Design Expert software. The model F-value (Table 7) of FLT, BT, D_{1h} , D_{6h} , and $t_{90\%}$ implied that the model were significant. There was only a 0.01% chance that a "model F-value" large could occur due to noise. FLT, BT, D_{1h} , D_{6h} , and $t_{90\%}$ had

TABLE 5: KINETIC MODELING OF DRUG DISSOLUTION PROFILE

Parameters	F1	F2	F3	F4	F5	F6	F7	F8	F9
Zero order									
k _o	13.997	12.669	12.615	11.723	10.336	10.257	9.833	9.274	8.579
R ² _adj	0.7987	0.8039	0.8879	0.7493	0.8423	0.8665	0.7061	0.8263	0.8299
AIC	67.8001	75.9339	71.1727	86.7348	89.9611	88.1433	105.402	98.4581	96.2129
MSC	0.6706	0.7909	1.4533	0.5549	1.1766	1.3700	0.4822	1.1121	1.1364
First order									
k,	0.306	0.280	0.266	0.273	0.218	0.213	0.230	0.192	0.164
R ² _adj	0.9587	0.9622	0.9645	0.9536	0.9394	0.9540	0.9461	0.9450	0.9616
AIC	53.5540	59.4602	59.6729	68.1689	78.4788	75.3478	83.3635	83.5091	76.8539
MSC	2.2535	2.4383	2.6033	2.2427	2.1334	2.4363	2.1775	2.2620	2.6256
Higuchi model									
k _u	33.909	32.421	32.050	31.640	28.963	28.696	28.999	27.127	25.099
R ² _adj	0.9908	0.9919	0.9842	0.9929	0.9778	0.9805	0.9901	0.9819	0.9875
AIC	40.0059	44.1258	51.6087	47.4962	66.4048	65.0898	61.3317	69.0613	62.2470
MSC	3.7589	3.9718	3.4097	4.1220	3.1396	3.2912	3.8723	3.3734	3.7492
Hixson-Crowell									
k _{нс}	0.081	0.074	0.071	0.071	0.058	0.057	0.060	0.051	0.045
R ² _adj	0.9487	0.9567	0.9737	0.9403	0.9433	0.9606	0.9291	0.9429	0.9506
AIC	55.5008	60.8266	56.6843	70.9442	77.6797	73.4943	86.9112	84.0012	80.1271
MSC	2.0372	2.3017	2.9021	1.9904	2.2000	2.5908	1.9046	2.2242	2.3738

AIC: Akaike Information Criterion, MSC: model selection criterion

TABLE 6: KINETIC MODELING OF DRUG DISSOLUTION PROFILE BY KORSMEYER-PEPPAS	MODEL
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Parameter	F1	F2	F3	F4	F5	F6	F7	F8	F9
K _{kp}	33.434	31.176	26.476	32.466	25.131	23.821	30.683	24.039	22.214
n	0.509	0.522	0.608	0.486	0.573	0.595	0.472	0.559	0.560

TABLE 7: SUMMARY OF ANOVA TABLE FOR DEPENDENT VARIABLES FROM 3² FACTORIAL DESIGN

Source	Sum of squares	df	Mean square	F	Р	Remark
					Prob > F	
FLT (quadratic)						
Model	68158.12	5	13631.62	703.78	<0.05	Significant
Residual	77.48	4	19.37			
Lack of fit	69.48	3	23.16	2.89	0.4020	Not significant
Pure error	8.00	1	8.00			
BT (quadratic)						
Model	73147.78	5	14629.56	434.69	<0.05	Significant
Residual	134.62	4	33.65			
Lack of fit	84.62	3	28.21	0.56	0.7248	Not significant
Pure error	50.00	1	50.00			
D _{1h} (linear)						
Model	115.57	2	57.78	137.39	<0.05	Significant
Residual	2.94	7	0.42			
Lack of fit	2.49	6	0.42	0.92	0.6625	Not significant
Pure error	0.45	1	0.45			
D _{6b} (quadratic)						
Model	610.23	5	122.05	139.79	<0.05	Significant
Residual	3.49	4	0.87			
Lack of fit	2.89	3	0.96	1.59	0.5142	Not significant
Pure error	0.60	1	0.60			
t _{90%} (interaction)						
Model	26.74	3	8.91	89.58	<0.05	Significant
Residual	0.60	6	0.100			
Lack of fit	0.60	5	0.12	1973.44	0.0171	Significant
Pure error	6.050	1	6.050			

FLT: floating lag time, BT: buoyancy time; t₉₀₈: time required to 90% drug release, D₁₀: percentage of drug release in 1 h, D_{6h}: percentage of drug release in 6 h

"Prob>F" less than 0.0500 indicating model terms are significant. FLT, BT, D_{1h} , D_{6h} had non Significant lack of fit that implied polynomial model fits all design points well. R², Adj R², Pred R² (Table 8) value above 0.60 implies that the design expert model run for floating sustained release matrix tablet statistically significant and that can be utilize for modeling the design space^[22,23].

The application of response surface methodology yielded the following regression equations which are an empirical relationship between the logarithmic values of FLT, BT, D_{1h} , D_{6h} , and $t_{90\%}$. Test variables in coded units: FLT=+227.14+99.50A+35.83B-4.50AB-19.79A²+8.21B²; BT=+713.43+109.50A+8.17B+5.50AB-13.36A²-8.36B²; D_{1h} =+34.01-1.74A-4.03B; D_{6h} =+67.90-8.73A-4.46B-0.87AB+1.58A² + 2.97B²; $t_{90\%}$ =+9.34+1.81A+0.97B+0.59AB.

TABLE 8: STATISTICAL PARAMETERS

Parameters	FLT	BT	D _{1h}	D _{6h}	t _{90%}				
SD	4.40	5.80	0.65	0.93	0.32				
Mean	220.20	700.40	34.01	70.63	9.34				
CV %	2.00	0.83	1.91	1.32	3.38				
PRESS	538.81	877.64	5.85	21.34	1.27				
R ²	0.9989	0.9982	0.9752	0.9943	0.9782				
Adjusted R ²	0.9974	0.9959	0.9681	0.9872	0.9672				
Pred R ²	0.9921	0.9880	0.9507	0.9652	0.9535				
Adeq precision	79.397	52.370	32.488	36.448	27.881				

FLT: floating lag time, BT: buoyancy time; $t_{90\%}$: time required to 90% drug release, SD: standard deviation, CV: coefficient of variation, PRESS: predicted residual sum of square

The polynomial Equation can be used to draw conclusions after considering the magnitude of coefficient and the mathematical sign it carries, (i.e. positive or negative). The positive sign indicate that there is positive reletionship between independent and dependent varibles, and vice a versa. Three-dimensional (3D) response surface plots (fig. 4) were constructed based on the model polynomial functions using Design Expert software. These plots are very useful to see interaction effects of the factors on the responses (dependent variables).

To optimize all the responses with different targets, a multi criteria decision approach like a numerical optimization technique by the desirability function and graphical optimization technique by the overlay plot were used (fig. 5). The optimized formulation was obtained by applying constraints on dependent variable responses. Optimized formulation was selected based on the criteria of 30-35% of the drug released at 1 h (D_{1h}), 60-65% of the drug released at 6 h (D_{6h}), and finally 90% of the drug released in between 10–11 h. The FLT and BT of floating sustained matrix tablet was omitted in the optimization process as they were not significantly affects the performance of formulation. These

constrains are common for all formulation. The recommended concentrations of the independent variables were calculated by the Design Expert software from the above plots which has the highest desirability near to 1.0. The optimized results obtained to give 39 solutions with therotical target profile characteristics and which were shown in Table 9.

Gastroretentive drug delivery system are promising doasge form for s (-) atenolol which could be a better alternative to the conventional dosage form in order to improve the bioavilability by increasing the gastric retention time of the drug and to minimize the side effect. The effervescent based floating drug delivery is promosing approach to achieve *in vitro* buoyancy by using gel forming polymer HPMC and gas generating agent sodium bicarbonate. s (-) atenolol floating tablets prepared by emplyoing 20% w/w HPMC K15M, 20% w/w HPMC K100 LV and 10% w/w



Fig. 4: Response surface plots.

Response surface plots showing the effect of concentration of HPMC K15M and HPMC K100LV on (a) floating lag time (b) buoyancy time (c) D_{1h} (d) D_{6h} (e) t90%.



Concentration of

HPMC K15M (%)

TABLE 9: SOLUTIONS PROPOSED BY DESIGN EXPERT SOFTWARE

D_{1h} (%) D_{6h} (%)

t_{90%} (h)

Concentration of

HPMC K100LV (%)

17.37	20.12	33.08	63.99	10.22
18.00	18.75	33.97	64.66	10.09
17.00	22.50	31.30	62.99	10.66
18.00	19.00	33.77	64.34	10.15
16.00	23.00	31.24	64.50	10.35
16.41	22.52	31.48	63.93	10.42
16.69	24.12	30.09	63.22	10.91
19.75	19.37	32.86	61.74	10.86
16.63	23.87	30.32	63.33	10.82
18.36	20.36	32.55	62.40	10.65
19.78	19.12	33.05	62.01	10.80
17.51	22.00	31.52	62.43	10.75
17.76	22.51	31.03	61.83	10.98
17.32	19.68	33.45	64.50	10.09
19.52	18.55	33.60	63.07	10.53
16.29	21.26	32.54	64.76	10.08
18.88	20.00	32.66	62.08	10.74
17.95	19.93	33.04	63.37	10.38
16.81	23.38	30.65	63.06	10.79
17.10	23.29	30.62	62.61	10.90
19.33	18.07	34.05	63.97	10.33
16.21	23.65	30.64	64.04	10.58
19.09	19.48	33.01	62.39	10.66
18.73	20.81	32.05	61.51	10.91
19.89	17.08	34.65	64.98	10.20
17.33	22.36	31.29	62.54	10.76
18.70	18.46	33.96	64.15	10.24
16.94	23.36	30.62	62.86	10.84
18.40	21.43	31.67	61.49	10.96
16.37	24.08	30.24	63.76	10.75
19.92	17.99	33.91	63.45	10.49
17.98	19.53	33.35	63.75	10.29
19.66	18.12	33.90	63.54	10.45
16.75	23.71	30.40	63.12	10.84
16.88	23.63	30.43	62.92	10.88
18.33	21.12	31.94	61.80	10.85
16.97	20.39	33.01	64.35	10.14
17.07	22.83	31.00	62.78	10.77
16.25	24.04	30.32	63.96	10.69

Fig. 5: Desirability plot and Overlay plot for optimization formulation.

(a) Desirability plot (b) Overlay plot for optimization of floating sustained release matrix tablet.

SB (Formulation F8) was the best formulation with *in vitro* floating time, buyoancy time and drug release. A systematic study using 3² factorial design revelead that concentration of HPMC K15M and HPMC K100 LV significantly affects the percentage drug release. HPMC K100 LV which has lower viscosity and fast swelling rate significantly reduces the initial drug release level while HPMC K15M which has higher viscosity compared to HPMC K100 LV helps in sustaining the drug release upoto 12 h.

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HPMC K15M: hydroxypropyl methylcellulose K15M, HPMCK100LV: hydroxypropyl methylcellulose K100LV, t_{901} : time required to 90% drug release, D_{1h} : Percentage of drug release in 1 h, D_{6h} : Percentage of drug release in 6 h

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There are no conflicts of interest.

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